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A Method to Define Profile Modification of Spur Gear and Minimize the Transmission Error

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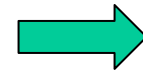
AVIO, Propulsione
Aerospaziale, Turin - Italy

Field of application

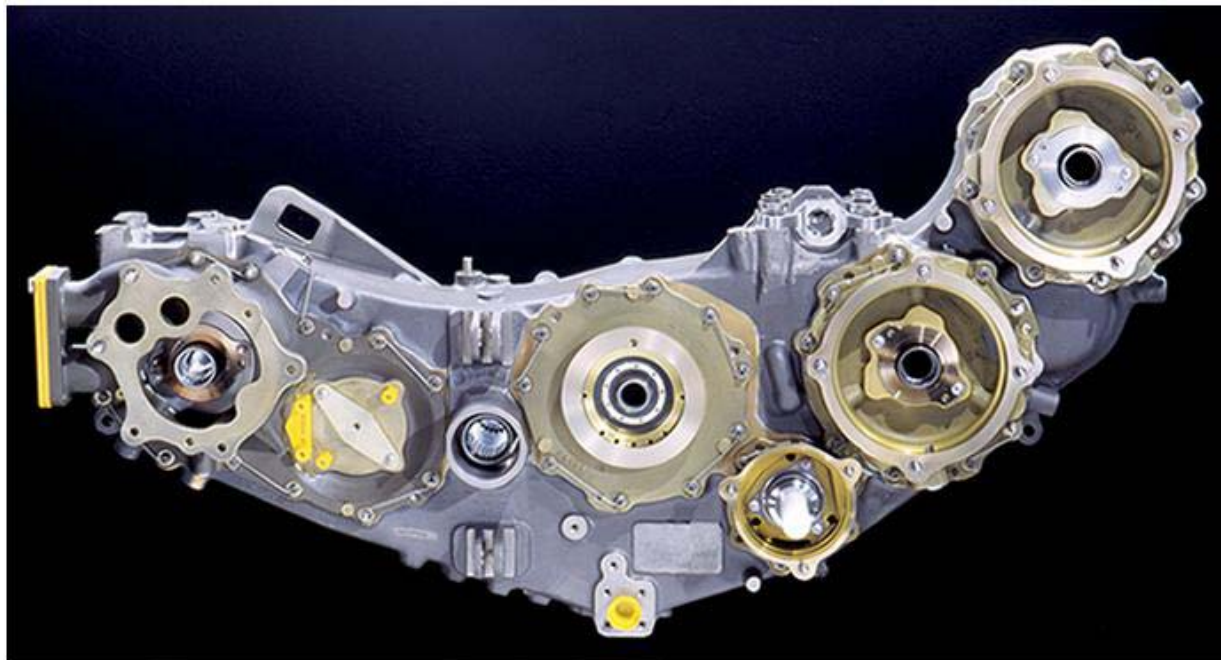
Aerospace applications Gear Boxes

- High performance
- Low weight

A very simple lay-out is needed



SPUR GEARS



Spur Gears Vs. Helical Gears

Advantages:

- Simpler assembly, no axial bearings



Spur Gear solution preferred

Disadvantages:

- Full impact at meshing start with spur gear
- Sharing factor function less smooth



Noise reduction needed

Causes of Noise with Spur Gear Transmissions

Transmission Error (TE) is considered to be the primary cause of whining noise, in Gear Boxes:

- [J.D. Smith](#). "Gears and theirs vibration, A Basic Approach to Understanding Gear Noise". *The Macmillan Press LTD.*, 1983.
- [G. Niemann](#), H. Winter. "Machinenelemente Band II, Getriebe allgemein, Zahnradgetriebe", vol. 2. *Grundlagen, Stirnradgetriebe, Springer-Verlag*. Berlin, 1983.

Definitions: Transmission Error

Transmission Error (TE) is defined as the difference between the effective and the kinematics position

TE is generated by:

- teeth spacing errors
- dynamic effects
- deflections induced by the load on teeth

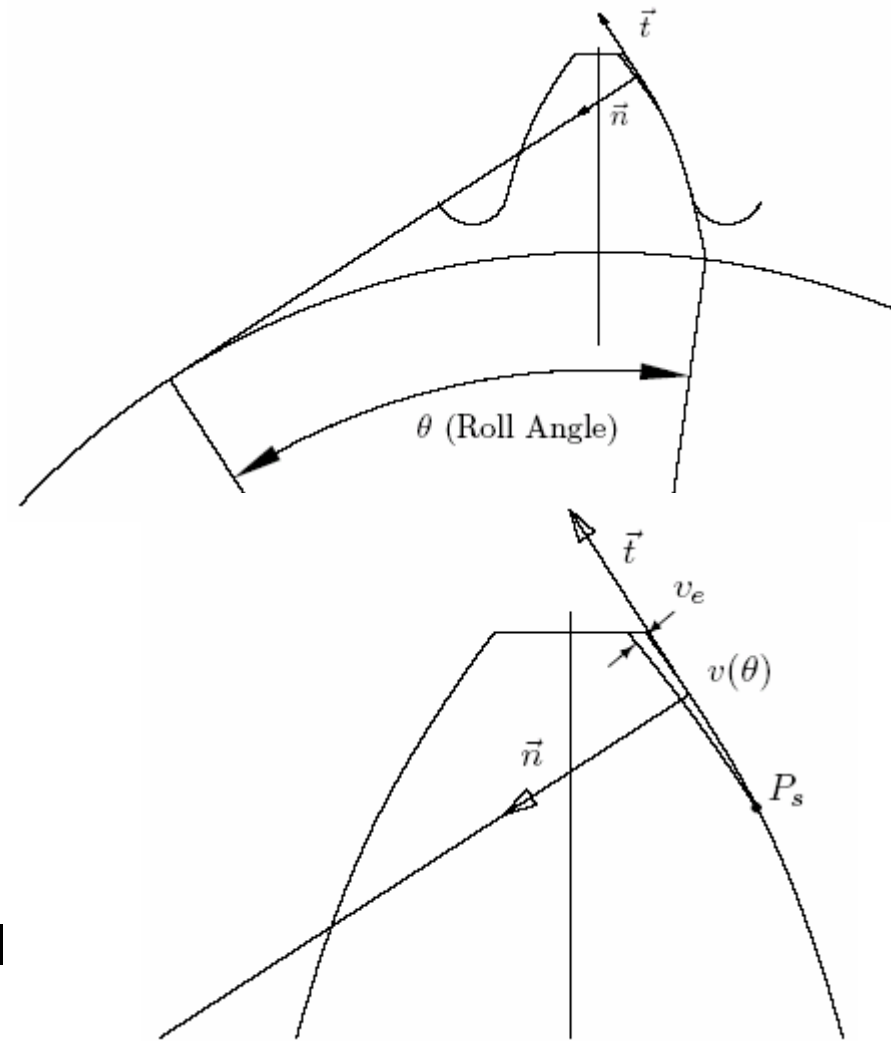
Peak to Peak Transmission Error (PPTE) is the difference between Maximum and Minimum of the TE trace

Profile modification (Tip Relief Modification) is a powerful design tool to interfere with TE

Definitions: Tip Relief Profile Modification

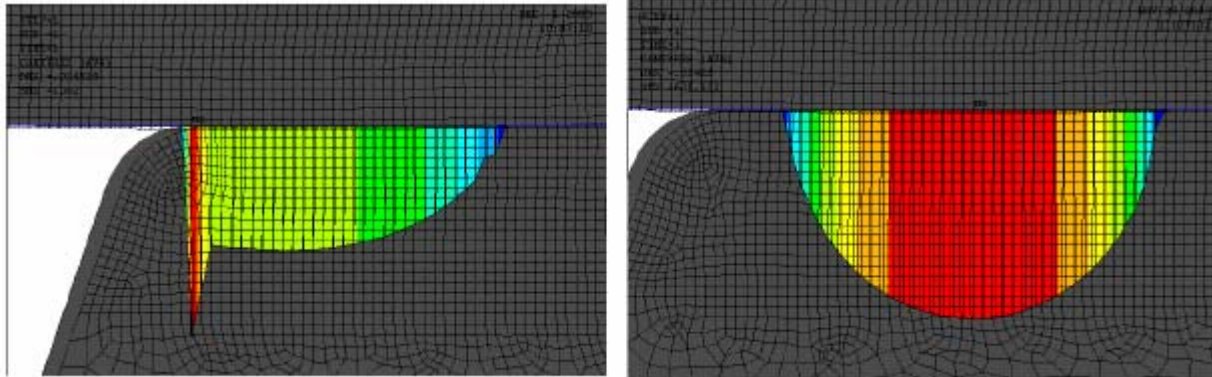
Profile modification definition:

- only at the tip
- definition along the involute nominal profile
- topography shape (ex. Linear or Parabolic)
- start relief Roll Angle θ
- total amount of material removal at the tip v_e

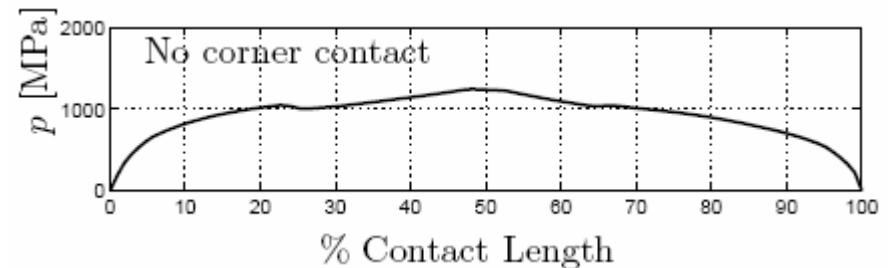
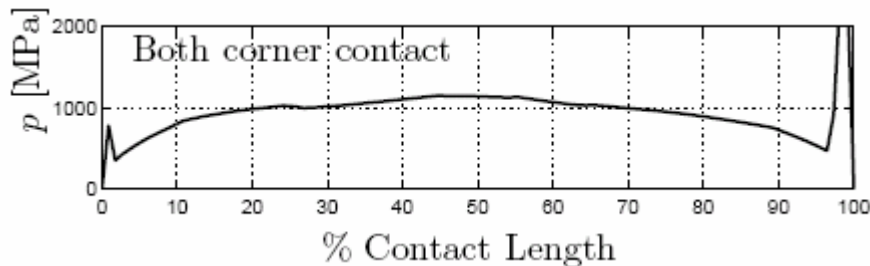


Definitions: Corner Contact

Corner Contact: Contact across the tip fillet,
if no fillet: complete Contact across the tip of the tooth



Maximum **Pressure** rises to very **high values** if Corn. Cont. appears



Corn. Cont. can be avoided with **adequate Tip Relief Modifications**

Aim of the paper

Noise and vibration optimization for a given spur gear set, both LCR and HCR are considered

PSTE is the function to minimize

Variables are: Profile **Topography shape**, Maximum amount of **material removal**, start relief **Roll Angles**

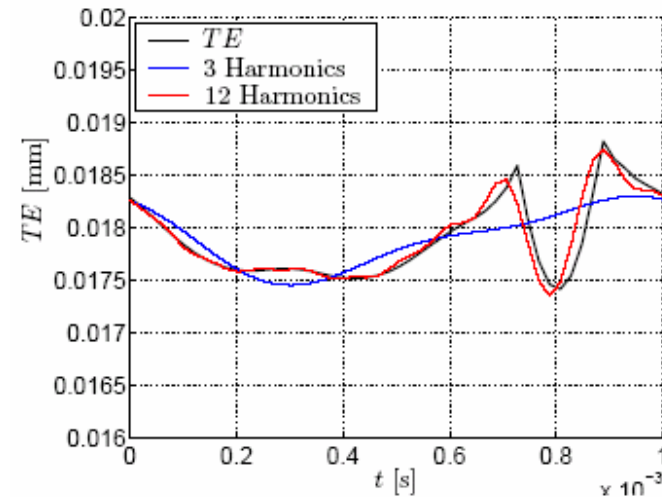
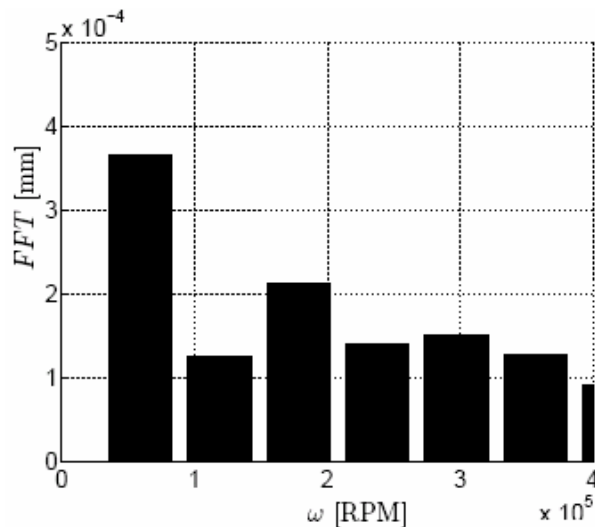
Boundaries are **Corner Contact** and **Pressure Maximum**.

Bending stress are too low sensitive to profile modification, even with HCR gear sets to be taken into account

Choices and parameters ranges

TE trace can be decomposed by FFT, to identify a function to minimize the sum of the first few harmonics can be considered

- M.S. Tavakoli and D.R. Houser. "Optimum profile modification for the minimization of static transmission errors of spur gears". *Proceedings of ASME 84 - DET - 173*, 1986.

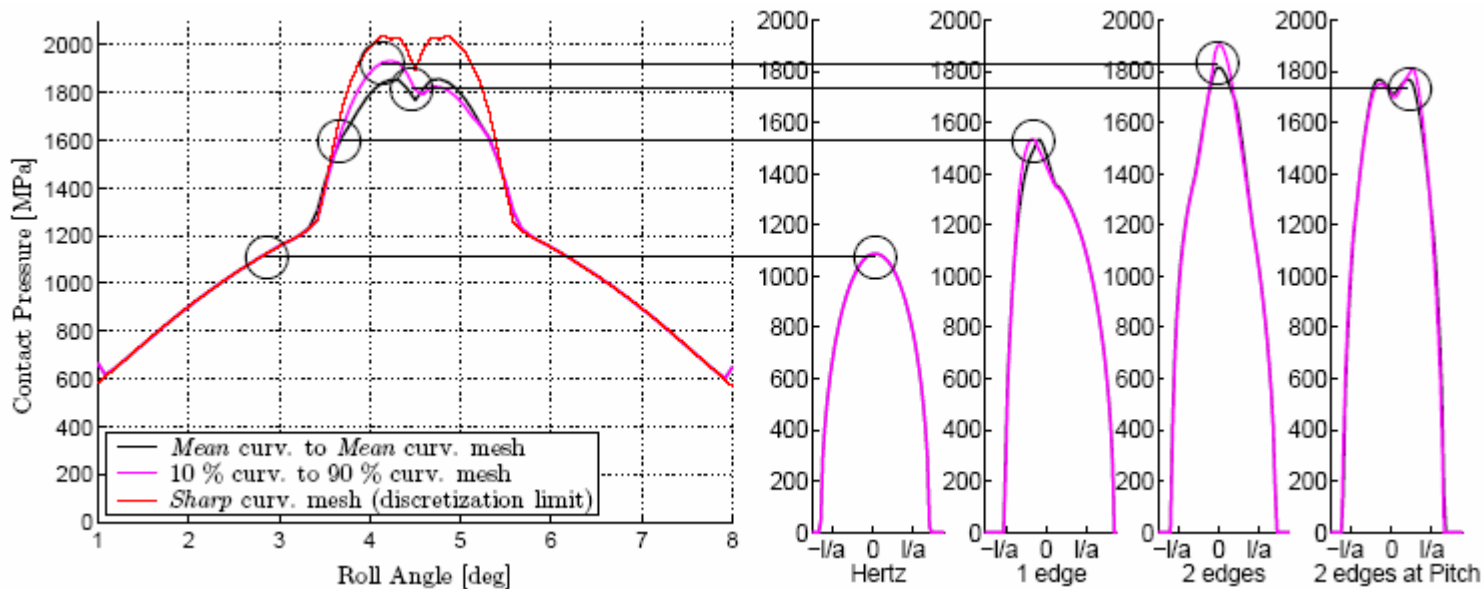


Few components cannot be the main part of the signal (like this)
PSTE is considered to have **better correlation** with whining noise

Choices and parameters ranges

Linear Tip relief generates a **sharp edge** at the start relief point then a **strong pressure rise**

- M.Beghini, G.M.Bragallini, F.Presicce, C. Santus. "Influence of the linear tip relief modification in spur gears and experimental evidence". *Proceedings ICEM12*. Bari, 2004.

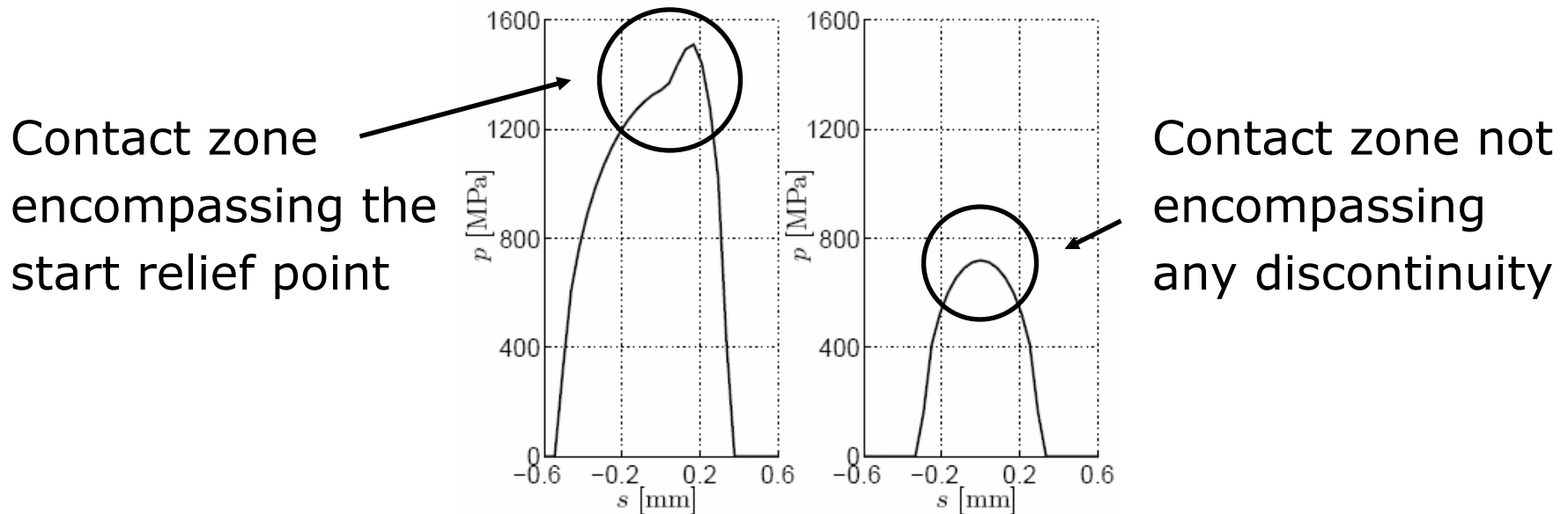


Parabolic Tip relief doesn't show this problem

Choices and parameters ranges

Parabolic Tip relief generates a **sharp** change of curvature but a **mild pressure rise** is produced.

- M.Beghini, C.Santus. "Analysis of plane contact with discontinuous curvature". *International Journal of Mechanical Sciences*. 2004. In Press.

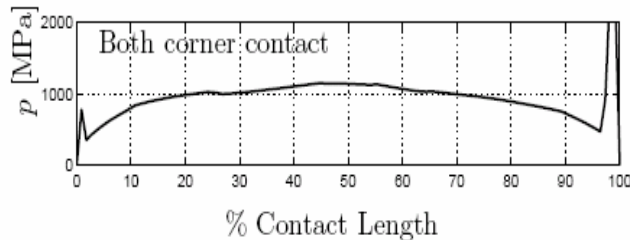


This kind of tip relief is accepted. Only **parabolic relief** is considered

Choices and parameters ranges

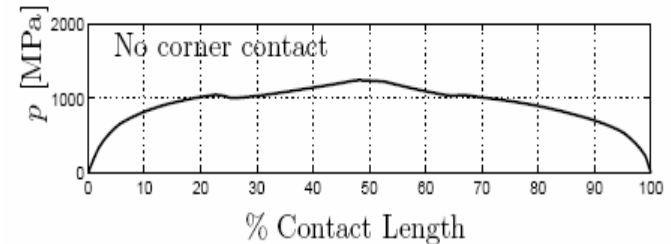
To assess the Total Amount Removal:

Gear Pair is simulated with **no Modification**
Corn. Cont. **found**



Niemann Rule,
increasing Tip
Relief Modif.

Gear Pair is simulated with **Modification** until
no Corn. Cont. is found



According to the **Niemann** rule the total amount is chosen to avoid the Corner Contact

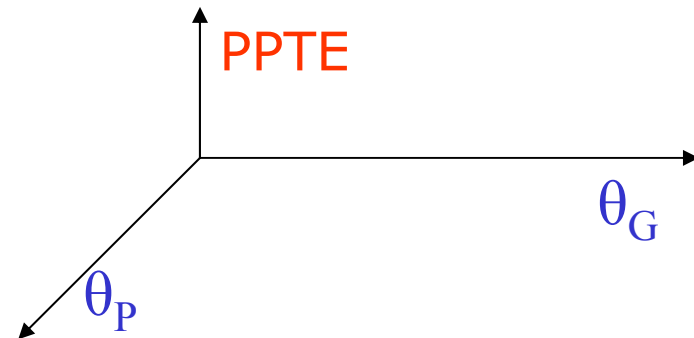
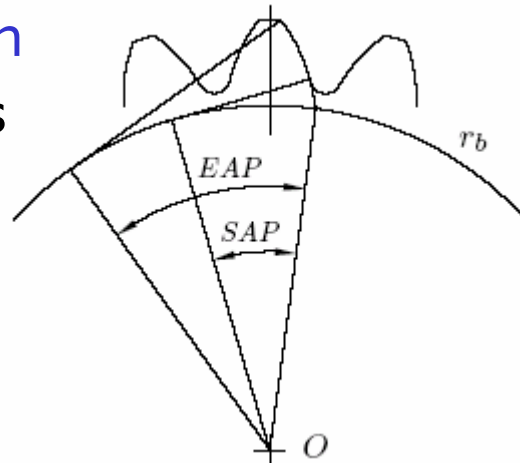
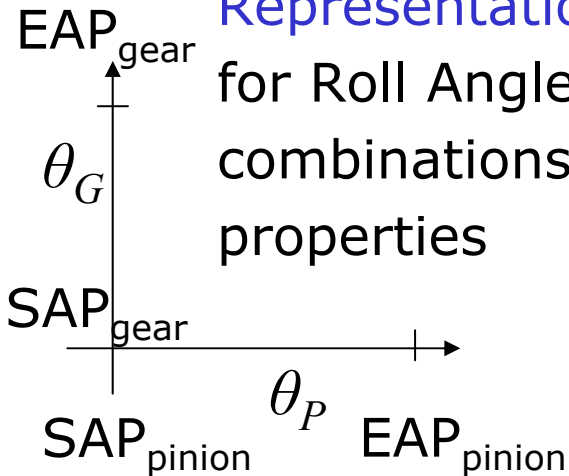
- **G. Niemann** and J. Baethge. "Transmission error tooth stiffness, and noise of parallel axis gears". *DIZ*, 112(4), 1970.
- **G. Niemann**, H. Winter. "Machinenelemente ...

Choices and parameters ranges

Start Relief Roll Angles are the Design Parameters left to perform the optimization

It is suggested a 3D map showing the PPTE vs. the 2 Start Relief Roll Angles Coordinates

Good Representation for Roll Angles combinations properties

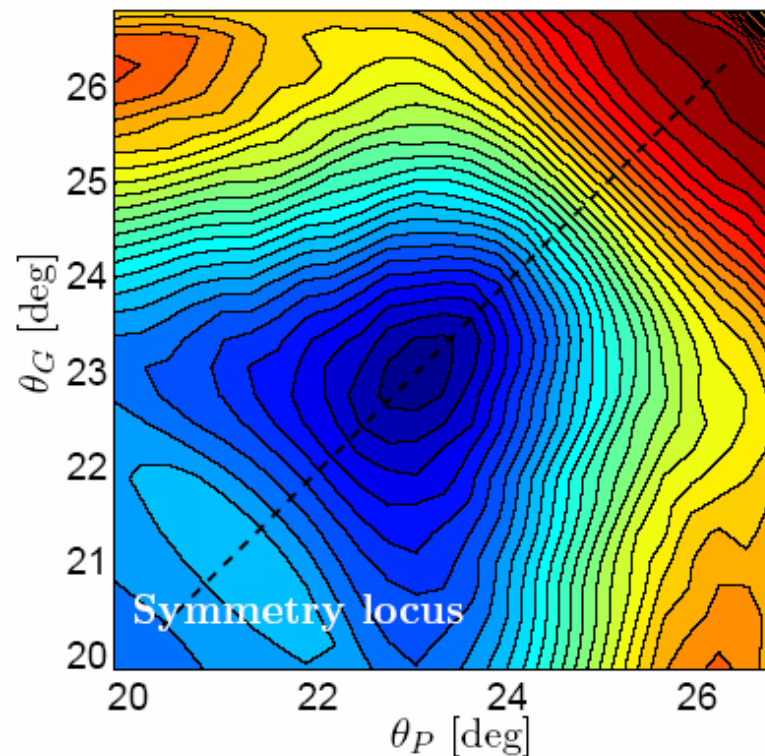
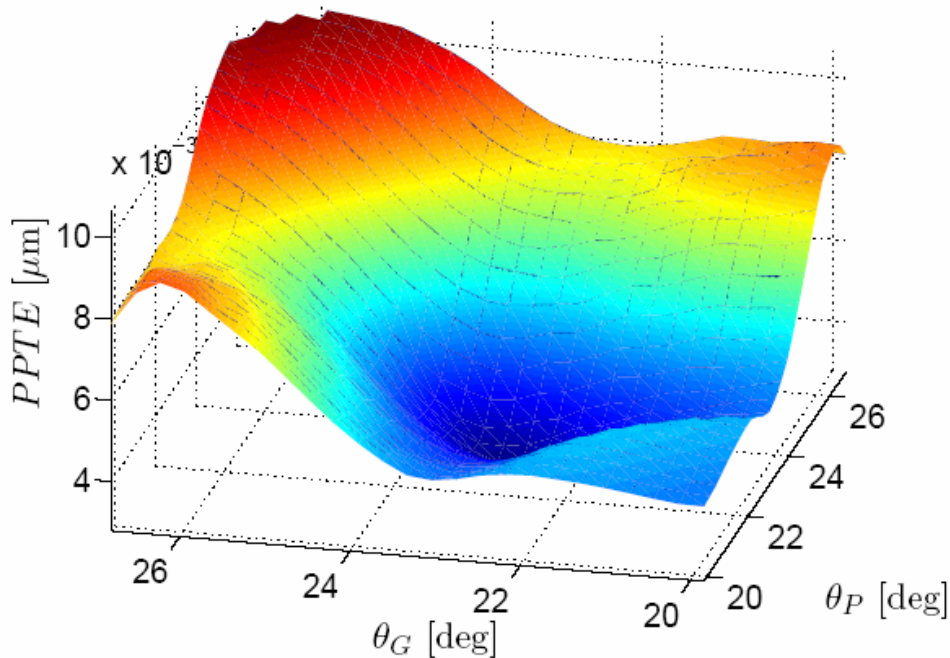


Immediate and intuitive Optimum Direct Search

Results: LCR Spur Gear Set

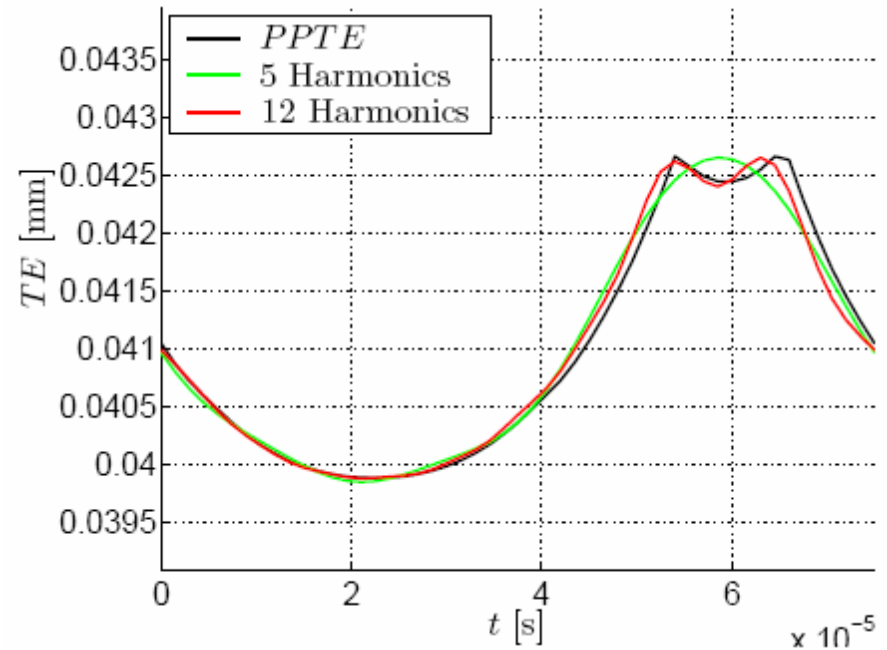
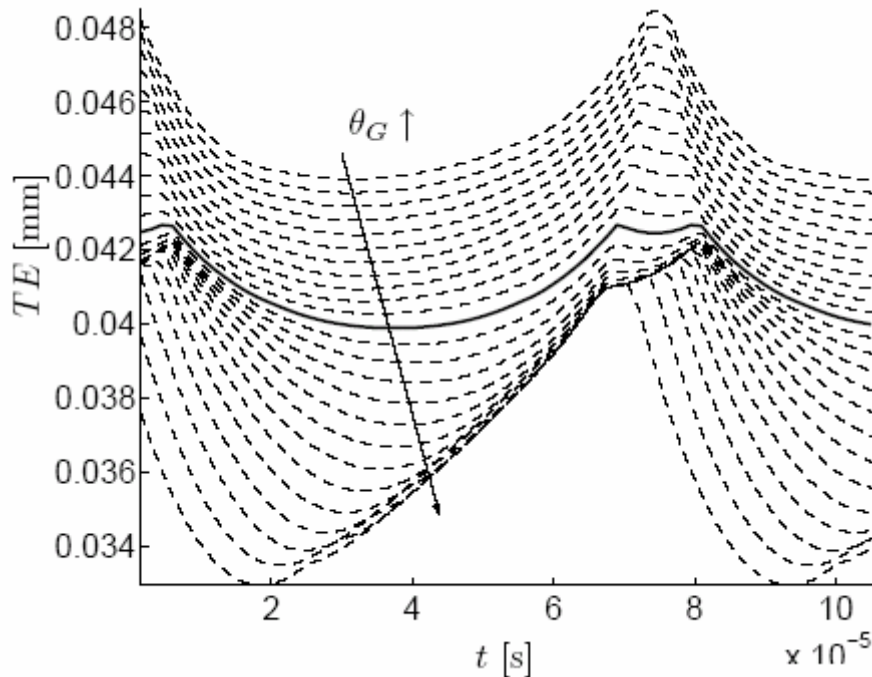
Equal teeth number Gear Set analyzed:

- Symmetry Locus
- Absolute Minimum found
- Local regularity at the absolute minimum



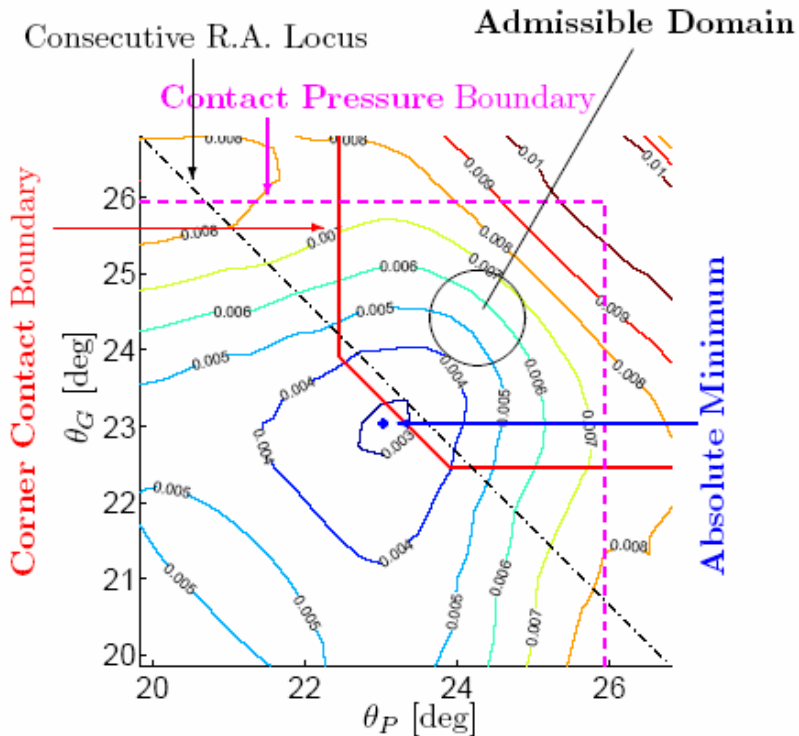
Results: LCR, properties of the minimum

- (θ_P, θ_G) minimum is **symmetric** for **equal teeth number**
- **parabolic** modification is easily recognizable
- change between 1 – 2 Contact Pairs have to be at the same level in the optimum **PSTE** trace

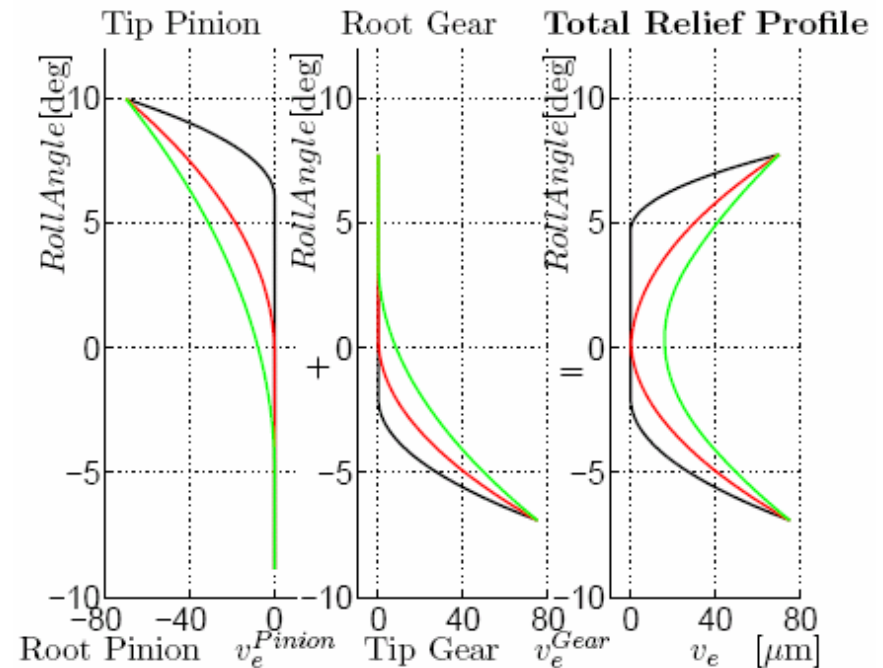


Results: LCR, application of boundaries

- (θ_P, θ_G) minimum falls out the **Corner Contact** boundary
- the other boundary is **not crucial**
- **Consecutive Roll Angle Locus** parallel to the **Corn. Cont.** bound. and near the **absolute minimum**



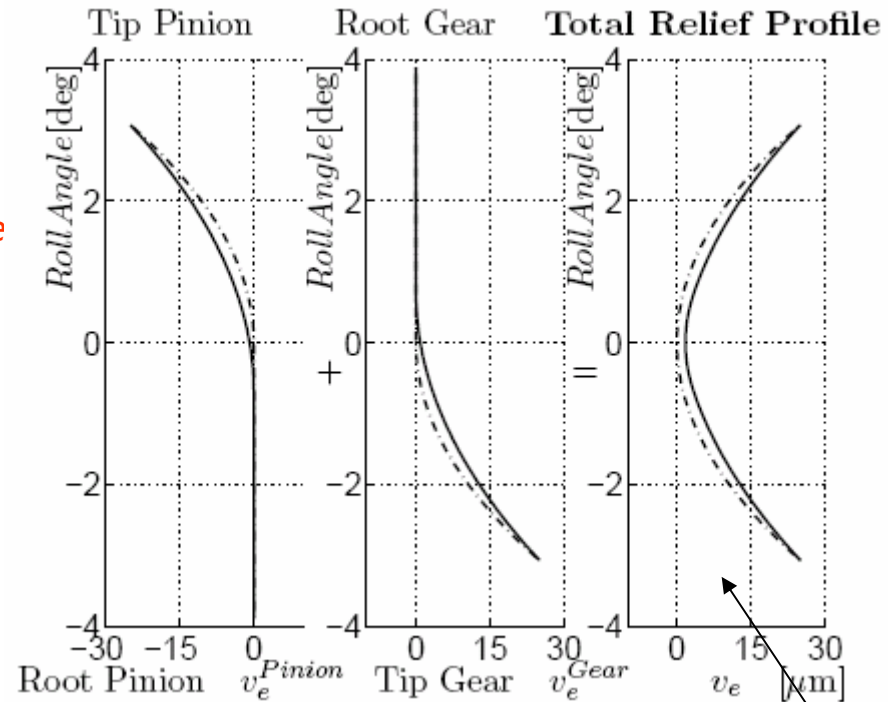
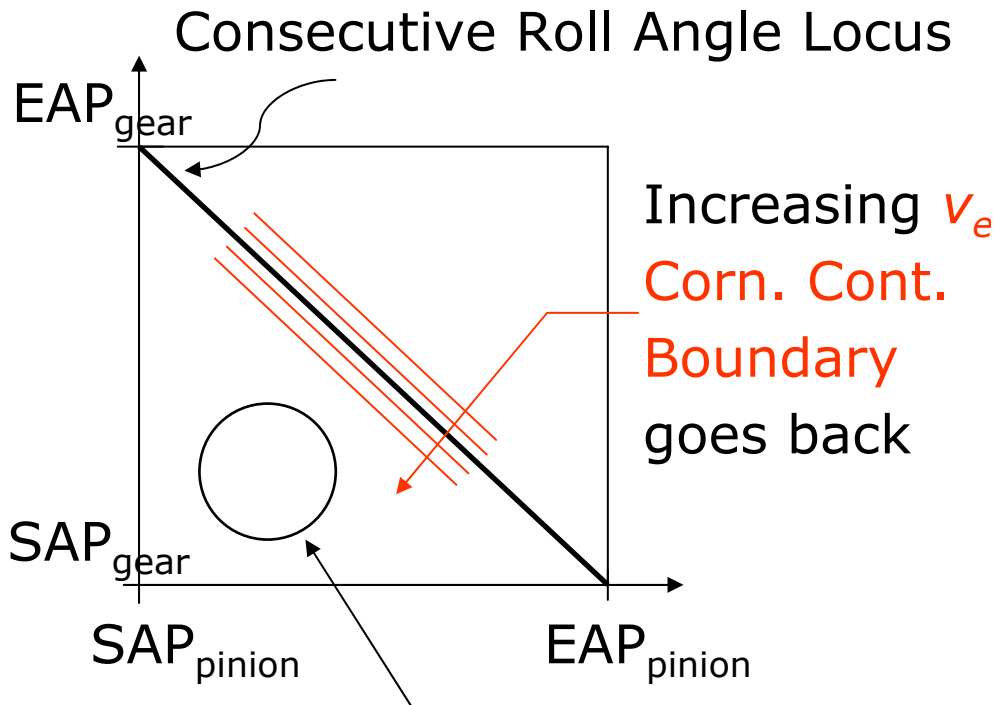
Consecutive Roll Angle Locus



Consecutive Start Relief Roll Angle Rule

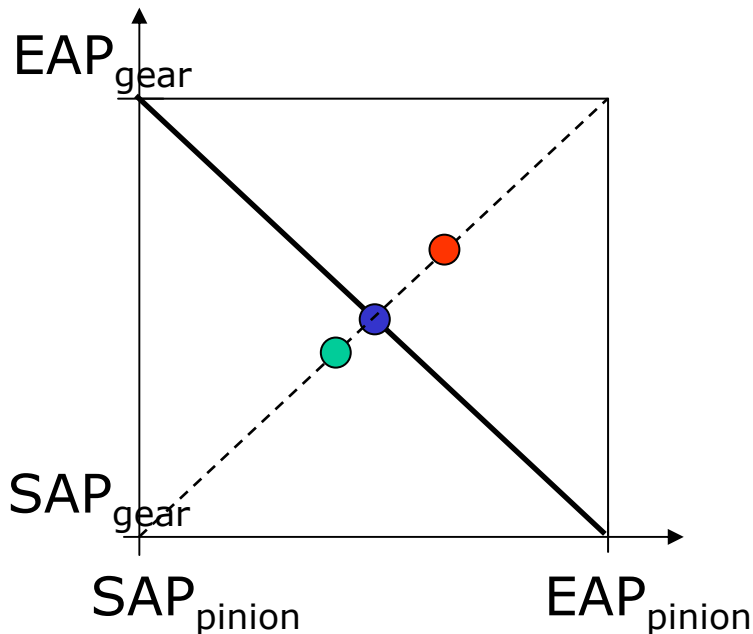
Definition of the **Consecutive Roll Angle Locus** and **Corner Contact Boundary**

Consecutive Roll Angle Locus vs. **Absolute minimum**



Roll Angle Overlapping, effective Total Amount reduced

Result of the optimization (LCR)



- Absolute Minimum
- Optimum Found
- Niemann Opt. (HPSTC)

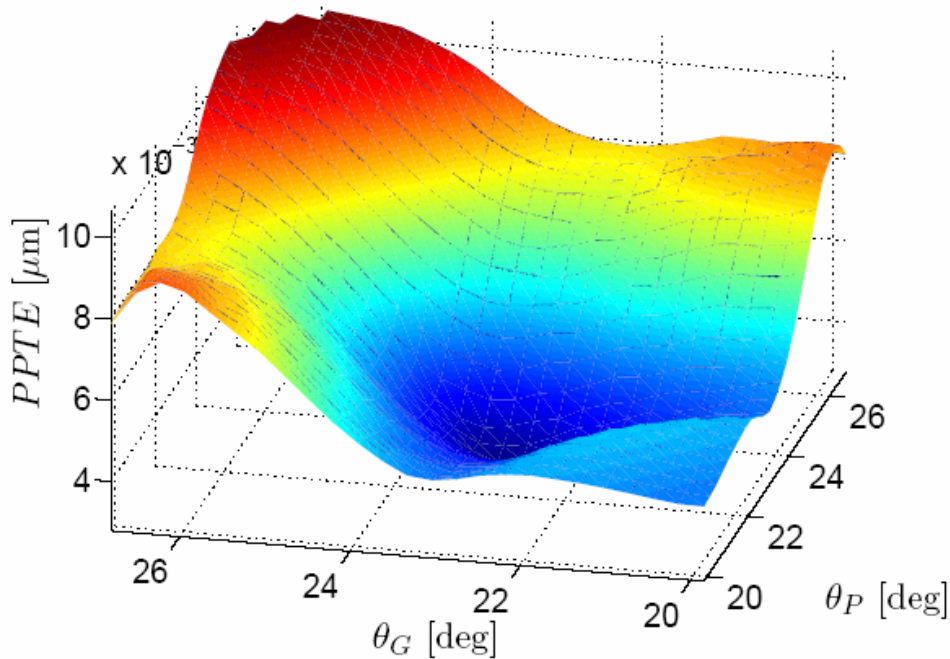
Niemann Suggestion is to start the profile modification at the **HPSTC** Point either for Pinion and Gear (Long Profile Modification)

Suggestion here proposed is an even **longer** modification:

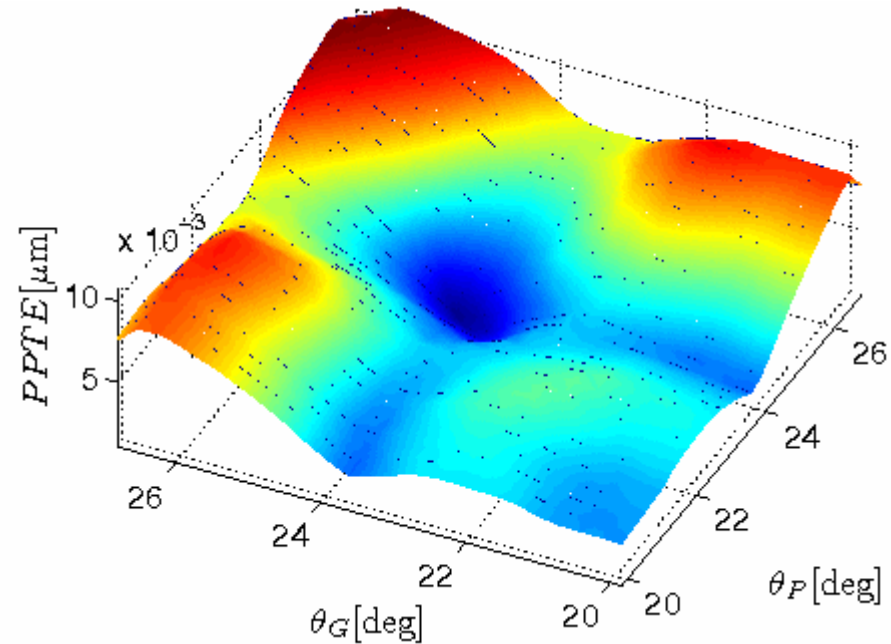
- the **whole** relative profile is modified (K-chart),
- **no involute-involute** point in contact is held.

Comparison with Linear modification

PPTe function with **Parabolic**
Tip Relief Modification



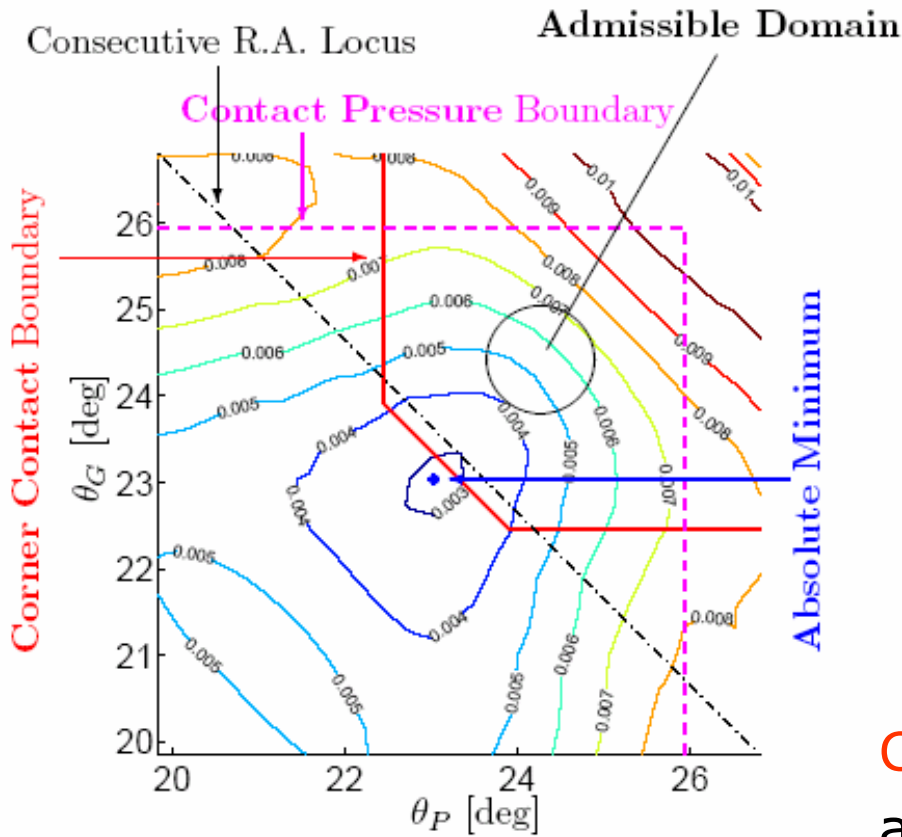
PPTe function with **Linear**
Tip Relief Modification



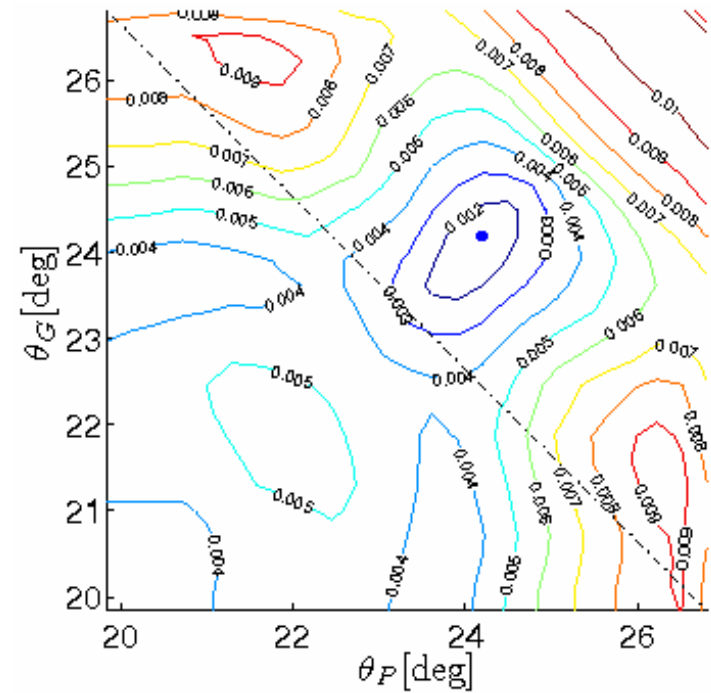
Linear shows the aforementioned **singular Contact Pressure**

Comparison with Linear modification

PPTe function with **Parabolic**
Tip Relief Modification



PPTe function with **Linear**
Tip Relief Modification

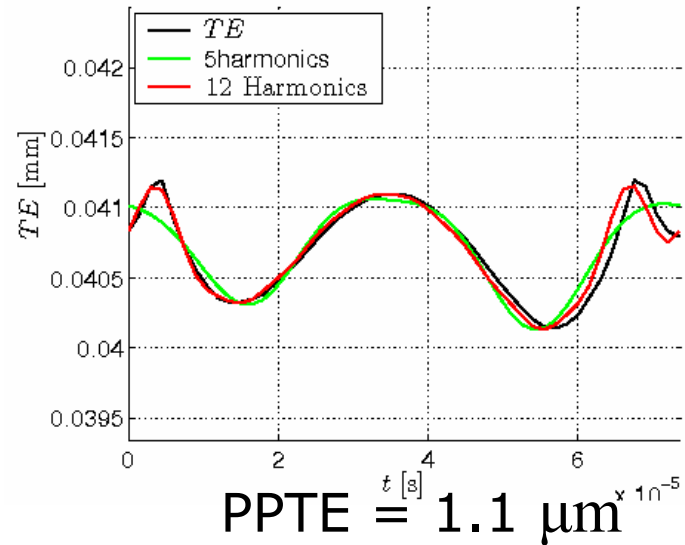
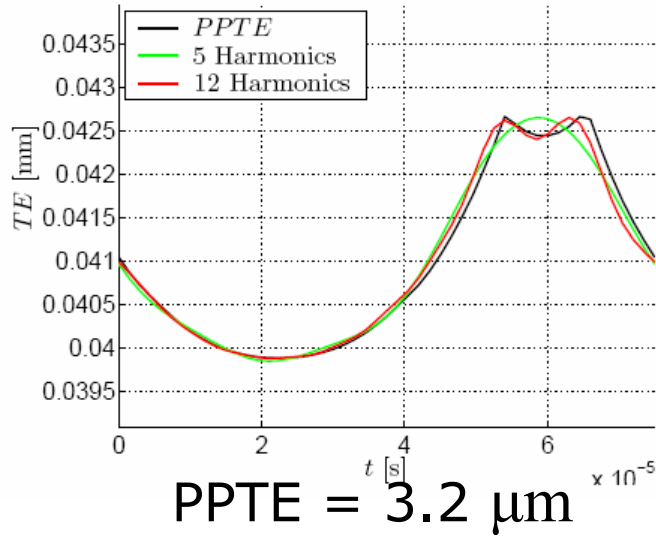


Consecutive Roll Angle does not
apply, **Niemann** rule more **effective**

Comparison with Linear modification

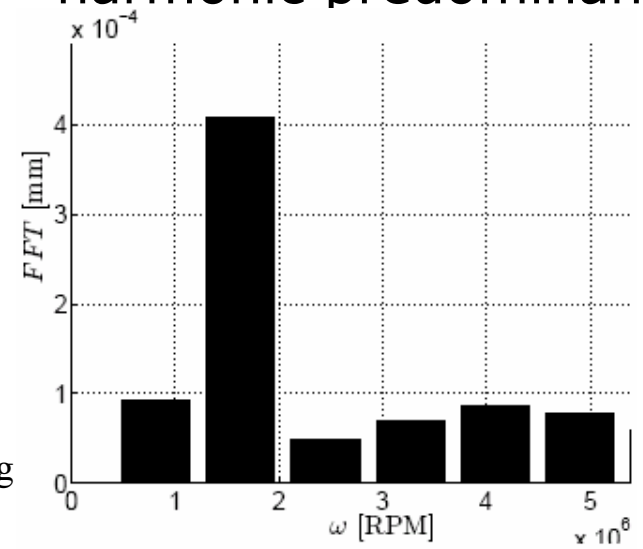
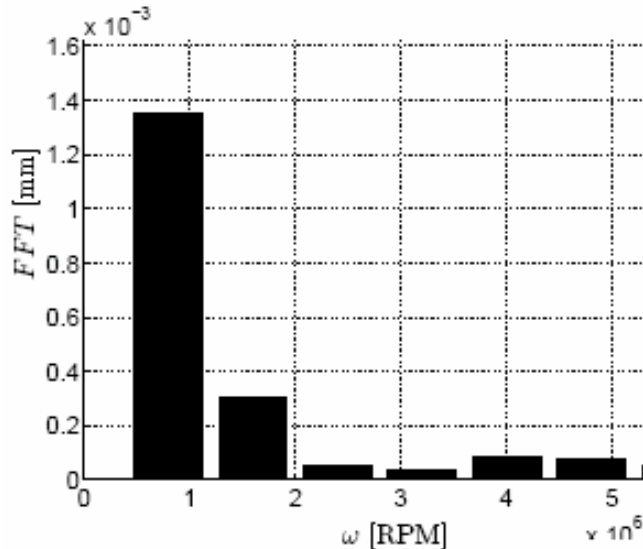
TE function with **Parabolic** Mod.

TE function with **Linear** Mod.



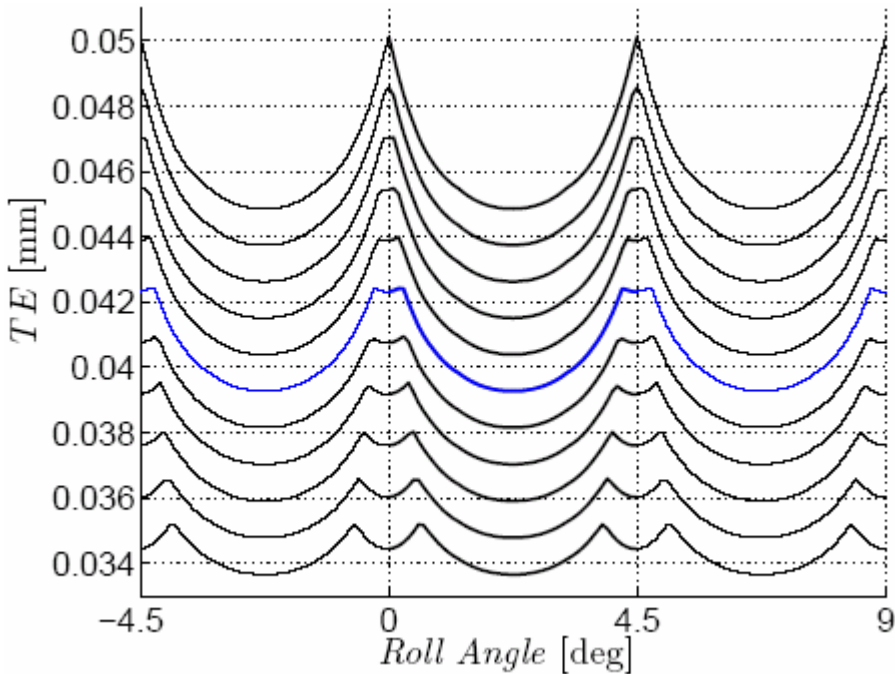
1st harmonic predominant

2nd harmonic predominant

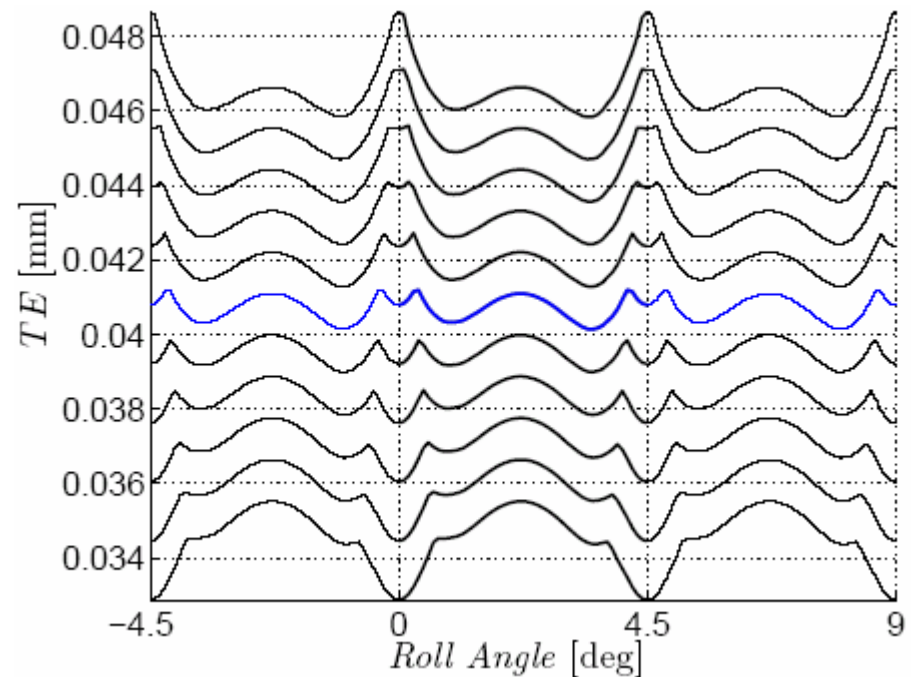


Comparison with Linear modification

TE function with **Parabolic** Tip Relief Modification



TE function with **Linear** Tip Relief Modification

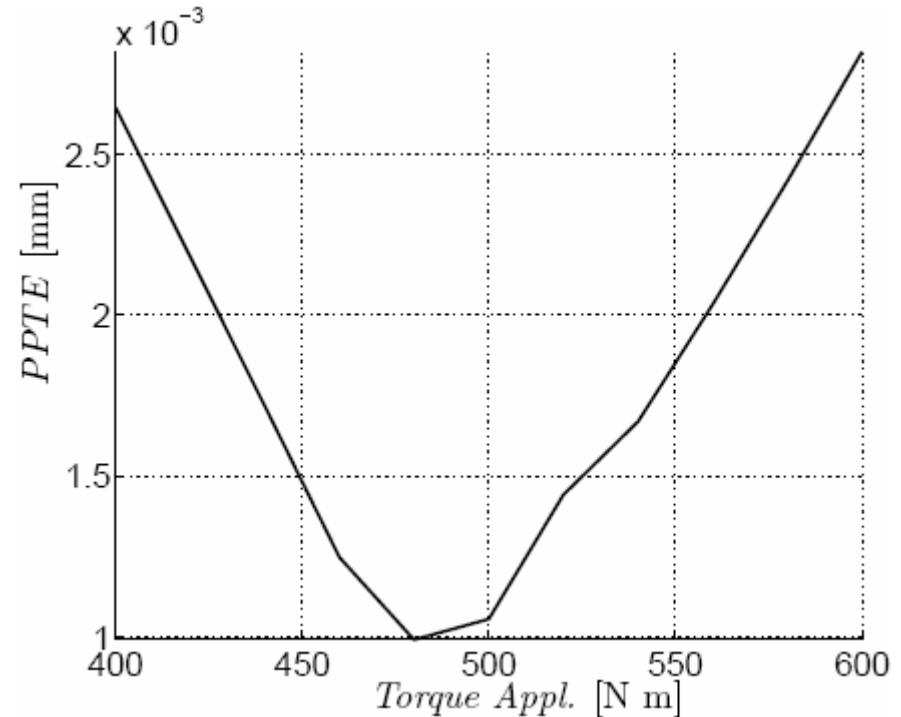
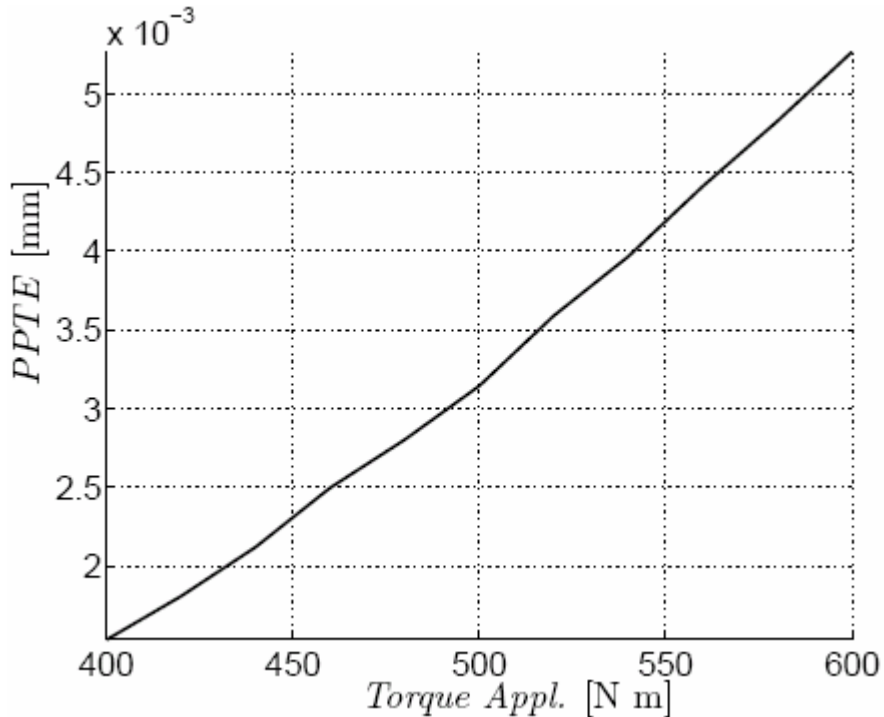


Different behavior in terms of TE **sensitivity** to the load

Comparison with Linear modification

PSTE(Torque) with **Parabolic** Tip Relief Modification

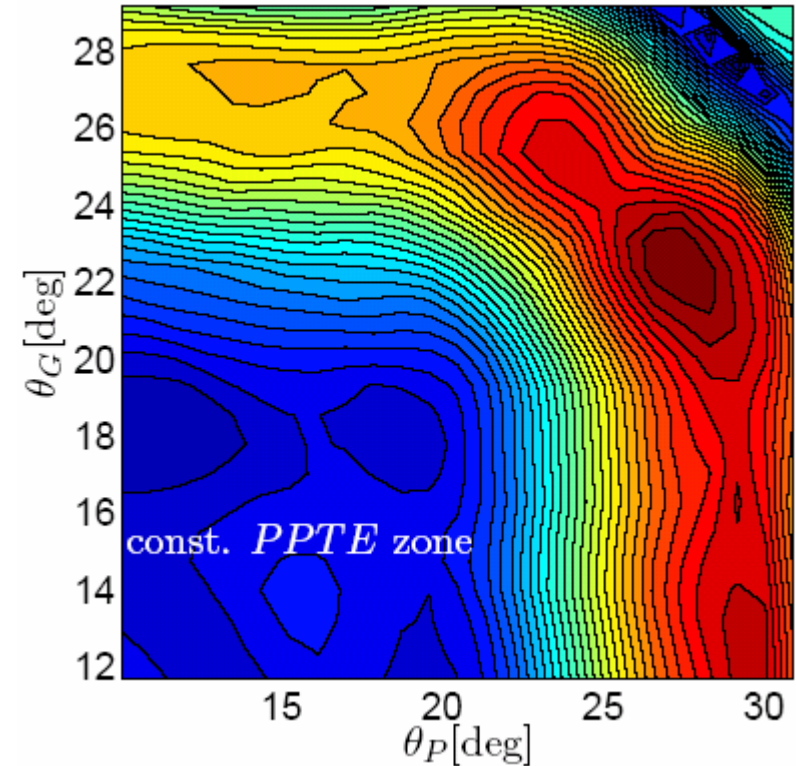
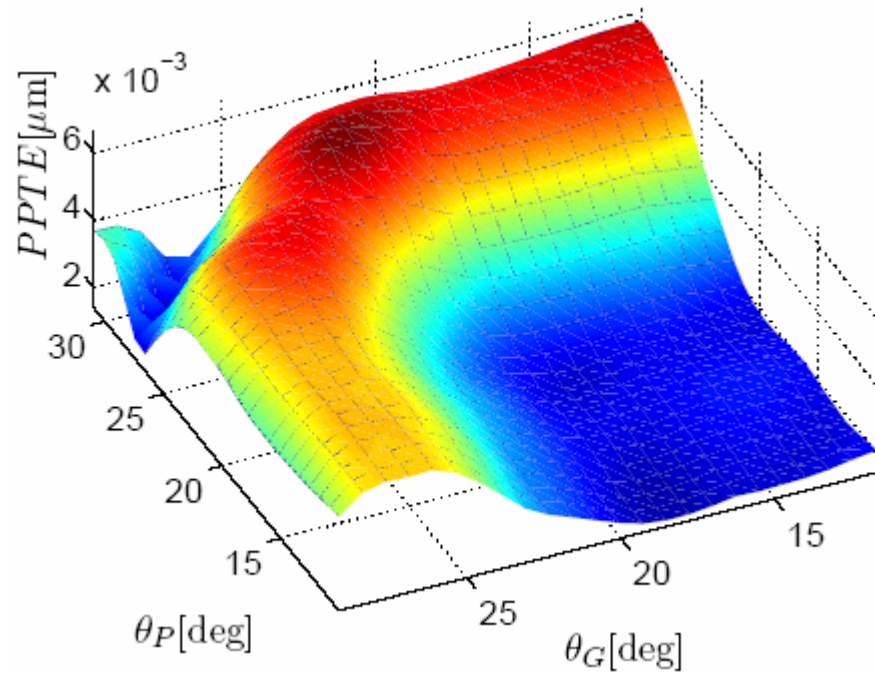
PSTE(Torque) with **Linear** Tip Relief Modification



Different behavior in terms of PSTE sensitivity to the load:

NO minimum with **Parabolic**, **Minimum** with **Linear**

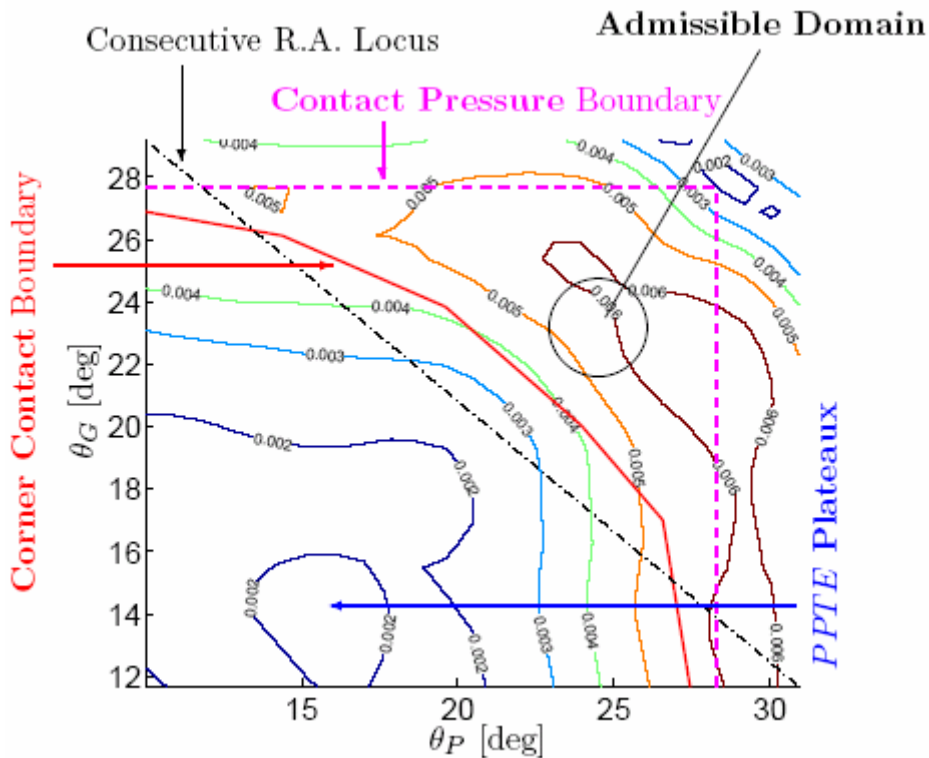
Results: HCR Spur Gear Set



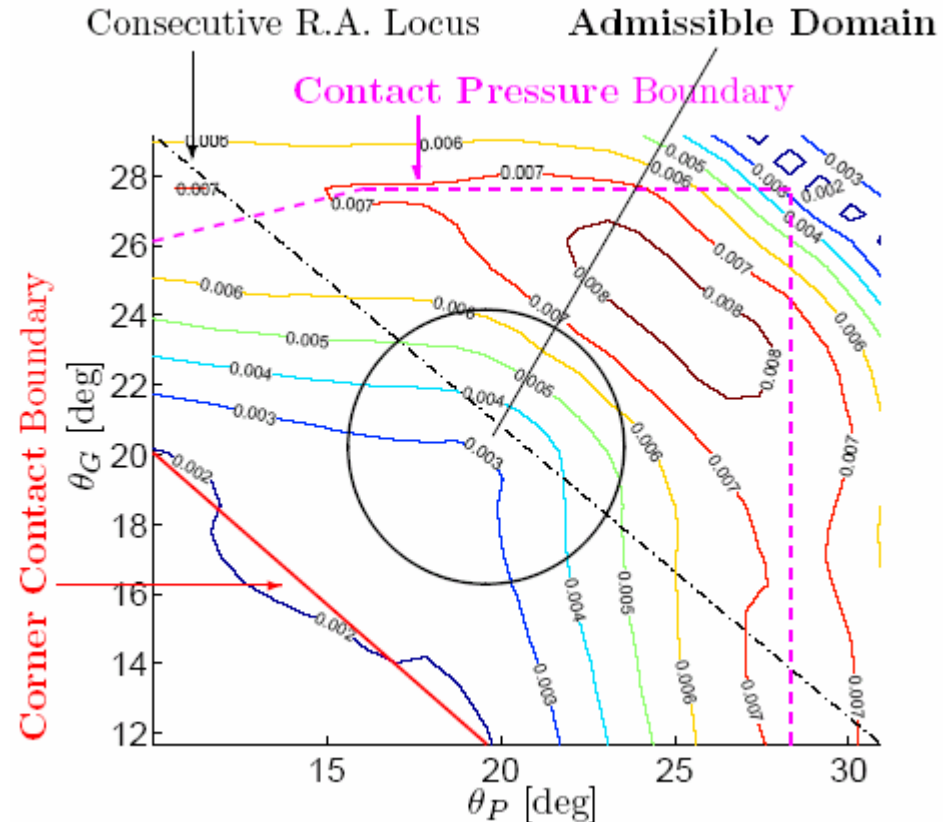
Results features:

- PPTe **Constant** at low Start Relief Roll Angle
- **Low** PPTe even at high Roll Angle

Results: HCR, application of boundaries



For HCR geometries **Corner Contact** boundary encompasses the whole part of the **PPTe plateaux** (v_e assessment)



By increasing the Total Amount v_e by a factor 1.5 the Consecutive Roll Angle Locus falls in the **admissible domain**

Conclusions

- An **optimization** method is here performed
- Corner Contact and Contact Pressure **Boundaries** are explained and applied to the optimization procedure
- Roll Angle vs. **PSTE** 3D maps are presented
- **Consecutive Start Relief Roll Angle** is introduced and mono-dimensional search, with **Parabolic** Modification, is performed
- **Parabolic** and **Linear** tip relief are compared:
 - Linear Mod. produces **lower** PSTE then Parabolic Mod.
 - Linear Mod. generates **singular** Contact Pressure at start relief point, and so it is not acceptable
 - with Parabolic Mod. first harmonic is the strongest, while with Linear Mod. second harmonic is the predominant
- Both **LCR** and **HCR** Gear Set are considered

Further Development

- To avoid **Contact Pressure singularity** and keep the linear shape, the **BEST** profile modification is linear with parabolic fillet.
- The **curvature** of the fillet is an interesting parameter to investigate
- **Other shapes** for Tip Relief Modification can be taken into account

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